

1 Utilisation of barium-modified analcime in sulphate removal: isotherms, kinetics
2 and thermodynamics studies

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13

1 **Abstract**

2 Analcime and commercial zeolite were employed as a precursor for preparing sorbent material
3 for SO_4^{2-} removal over barium modification. Three sorbents were prepared: barium-modified
4 analcime (ANA-Na-Ba), barium-modified acid-washed analcime (ANA-Ac-Na-Ba) and barium-
5 modified zeolite (ZSM5-Na-Ba). Of the prepared materials, ANA-Ac-Na-Ba was the most
6 efficient sorbent material for SO_4^{2-} removal, with a maximum sorption uptake of 13.7 mg g^{-1} at
7 room temperature. Batch sorption experiments were performed to evaluate the effect of initial
8 pH, initial SO_4^{2-} concentration, sorbent dosage, temperature and contact time of sorption.
9 Several isotherms were applied to describe the experimental results and Bi-Langmuir was found
10 to provide the best correlation for adsorption of SO_4^{2-} on ANA-Ac-Na-Ba. Kinetic studies were
11 applied for the most effective sorbent material, ANA-Ac-Na-Ba, and the results showed that the
12 sorption process follows pseudo-second-order kinetics.

13

14 **Keywords:** adsorption; sulphate; analcime; zeolite; chemical modification

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16

1 Introduction

Natural zeolites are crystalline-hydrated "tectoaluminosilicate" minerals with cage-like structures [1,2]. Zeolites have a three-dimensional framework consisting of SiO_4 and AlO_4 tetrahedral molecules linked with shared oxygen atoms. Zeolites have a large surface area and high cation exchange capacity (CEC). The isomorphous replacement of Si^{4+} by Al^{3+} produces a negative charge, which is balanced by exchangeable alkali and alkaline-earth metal cations (Na^+ , K^+ , Ca^{2+} etc.). These cations are exchangeable with certain cations in solutions such as Pb^{2+} , Cd^{2+} , Zn^{2+} and Ni^{2+} [2]. Zeolites are usually pretreated with sodium solution before usage, because the ion exchange capacity of zeolite tends to increase if just monovalent cations are present in zeolite materials [3,4]. Zeolites can adsorb variably sized ions, which indicates their use as a selective adsorbent for many pollutants, including dyes [5,6], organics [7,8], ammonium [9,10] and metal ions [3,11] from wastewaters.

Zeolites can be found in volcanic environments (under hydrothermal conditions), salt lakes and sediment layers. The most common types of zeolites are clinoptilolite, mordenite, dachiardite, analcime (ANA), phillipsite and heulandite. Recently, ANA has also been reported to be an adsorbent in the wastewater treatment [12–14]. ANA ($\text{NaAlSi}_2\text{O}_6 \cdot \text{H}_2\text{O}$) is produced as a waste material in the mining industry, with irregular channels formed from four-, six- or eightfold rings [15]. Because zeolite materials have a low affinity for anions, chemical modification is needed to apply sorbent for anionic sulphate removal [2,16,17]. To remove anions from water, it is possible to modify natural zeolites with cationic surfactants (e.g. tetramethylammonium, hexadecyltrimethylammonium (HDTMA) bromide, tetrabutylammonium bromide (TBAB), n-cetylpyridinium bromide (CPB)) [1, 18-22]. Surface modification using cationic surfactant can change the surface charge and functionality by adding complex hydrophobic groups for positively charged exchange sites [2].

1 In addition, it is also possible to modify natural zeolites using inorganic salts (e.g. NaCl, FeCl₃,
2 BaCl₂), which improves the sorption efficiency for anions [23,24]. The modification has been
3 reported to create for example an oxi-hydroxide adsorption layer on the surface and change the
4 surface charge from negative to positive [17,24]. Due to that, stable complexes with anions in
5 solution are formed. In this study, the BaCl₂ modification was expected to impregnate Ba in the
6 framework structure of zeolites and subsequently enable the surface precipitation or
7 complexation of sulphate.

8 Sulphate (SO₄²⁻) anion is a major pollutant that occurs in both natural waters and industrial
9 effluent, such as acid mine drainage and wastes from the chemical industry [25,26]. SO₄²⁻ mainly
10 results from the process of chemical weathering of sulphur-containing minerals (e.g. gypsum).
11 In addition, SO₄²⁻ is generated through the oxidation of sulphides and elemental sulphur [27,28].
12 Sulphur is a necessary element for many kinds of organisms. However, excess SO₄²⁻ can cause
13 an imbalance in the natural sulphur cycle [26–29]. In addition, SO₄²⁻ concentrations higher than
14 150 mg L⁻¹ can damage water pipes [30] and concentrations higher than 600 mg L⁻¹ can have
15 laxative effects and affect the taste of the water [26].

16 SO₄²⁻ is common in drinking water and many countries have not set guidelines for it because
17 it is only mildly hazardous [26,27]. In Finland, the SO₄²⁻ limit in drinking water is set at 250 mg
18 L⁻¹ [30]. Environmental agencies in many countries have set maximum SO₄²⁻ values of 250–1000
19 mg L⁻¹ in both mine drainage and industrial effluent [26]. Typically, domestic sewage contains
20 less than 500 mg L⁻¹ of SO₄²⁻ but especially in industrial wastewater the concentration of SO₄²⁻
21 can be several thousand mg L⁻¹ [29].

22 Some examples of established methods for the removal of SO₄²⁻ are chemical precipitation,
23 biological treatment, ion exchange, reverse osmosis, electrodialysis and adsorption [26,28,31].
24 However, these methods suffered from various limitations. For example, biological treatment
25 and ion exchange are expensive while precipitation (e.g. with lime) produces large amounts of
26 sludge [26]. Furthermore, low SO₄²⁻ concentrations cannot be removed by lime precipitation

1 due to the high solubility of the produced CaSO_4 [32]. Among the various available water
2 treatment technologies, adsorption may be preferred for SO_4^{2-} removal because it is a simple
3 and effective technique. In addition, adsorption can be used in a so-called hybrid system with
4 precipitation in which sulphate remaining after precipitation can be removed via adsorption.
5 The success of this technique largely depends on the development of an efficient adsorbent
6 [28,29,31]. Activated carbon [33], clay minerals [28,31], biomaterials [27,29], zeolites [35] and
7 some industrial solid wastes [36] have been reported as adsorbents for SO_4^{2-} removal.
8 However, there is still a need for alternative and locally available raw materials or industrial by-
9 products with which to make sorbents.

10 The aim of this study was to investigate the effect of modification of natural analcime (ANA)
11 to the sorption capacity for SO_4^{2-} removal from an aqueous solution. Commercial zeolite (ZSM5)
12 was used as a reference material. Batch sorption experiments were performed to evaluate the
13 influence of initial pH, initial SO_4^{2-} concentration, sorbent dosage, temperature and contact
14 time. The Langmuir, Freundlich, Dubinin-Raduschkevich, Temkin, Bi-Langmuir, Sips, Redlich-
15 Peterson and Toth isotherm models were applied to the experimental data. Kinetic studies were
16 performed using pseudo-first-order, pseudo-second-order and Elovich kinetic models.

17

1 2 Materials and methods

2 2.1 Materials

3 Analcime (ANA) was obtained from a Finnish mining company. Commercial zeolite (NH₄-ZSM-5,
4 30:1 SiO₂:Al₂O₃, CAS: 1318-02-1) was used as a reference material (Alfa Aesar). Before use, all
5 materials were dried overnight at 110°C, crushed and sieved to obtain a particle diameter less
6 than 150 µm and to ensure a uniform product quality. The barium used in the modification was
7 BaCl₂. SO₄²⁻ ion stock solutions were prepared by dissolving of Na₂SO₄ (VWR 99.9 %) in MilliQ
8 water to generate a concentration of 5 g L⁻¹ and the mixture was diluted with distilled water
9 when necessary.

10 2.2 Characterisation methods

11 X-ray diffraction (XRD, PanAnalytical Xpert Pro) analysis was done for the untreated analcime
12 and zeolite samples to identify the mineral type. In addition, the produced sorbent materials
13 were characterized by XRD. X-ray fluorescence (XRF, PanAnalytical Minipal 4) analysis was
14 carried out to determine the chemical compositions of untreated samples. Fourier Transform
15 Infrared Spectroscopy (FTIR) spectra of the sorbent were collected using a Perkin Elmer
16 Spectrum One spectrometer equipped with an Attenuated Total Reflectance (ATR) unit. The
17 specific surface areas, pore sizes and pore volumes of samples were determined from nitrogen
18 adsorption desorption isotherms at the temperature of liquid nitrogen (-196 °C) using a
19 Micromeritics ASAP 2020.

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22

1 **2.3** Preparation of sorbents

2

3 Modification of analcime and zeolite was performed using two different protocols. By the
4 protocol 1, analcime and zeolite were treated with NaCl and after that with BaCl₂ [37]. In the
5 protocol 2, analcime was acid (HCl) washed before NaCl and BaCl₂ treatment.

6 *Protocol 1:* Analcime and ZSM-5 (5 g) was mixed with 1 M NaCl solution (50 mL) for 24 h,
7 rinsed with deionised water and dried at 105 °C to ensure that all ion exchange sites were in Na
8 form. The barium modification was done by mixing the material (5 g) with 1 M BaCl₂ solution
9 (100 mL) for 16 h, rinsing with deionised water and drying at 105 °C. The materials were stored
10 in a desiccator prior to use.

11 *Protocol 2:* Analcime (5 g) was acid washed with 2 M HCl (100 mL) for 24 h, rinsed with
12 deionised water and dried 105 °C. Next, the analcime was mixed with 2 M NaCl solution (50
13 mL) for 24 h, rinsed with deionised water and dried at 105 °C to ensure that all ion exchange
14 sites were in Na form. The barium modification was done by mixing the material (5 g) with 1 M
15 BaCl₂ solution (100 mL) for 16 h, rinsing with deionised water and drying at 105 °C. The materials
16 were stored in a desiccator prior to use.

17 **2.4** Batch sorption experiments

18 In the sorption experiments, the effects of initial pH, initial SO₄²⁻ concentration, sorbent dosage,
19 temperature and contact time on the removal efficiency of SO₄²⁻ over Ba-modified analcime
20 (ANA-Na-Ba), Ba-modified acid-washed analcime (ANA-Ac-Na-Ba) and Ba-modified commercial
21 zeolite (ZSM5-Na-Ba) were studied. The observed sorption conditions are presented in Table 1.
22 Kinetic studies were performed in a 1 L reactor vessel equipped with a magnetic stirrer with an
23 agitation speed of 1000 rpm.

24

1 Table 1. Parameters for testing the effects of initial pH, initial SO_4^{2-} concentration, sorbent
 2 dosage, contact time and temperature on SO_4^{2-} removal from synthetic solution.

Parameter	Sorbent	Initial pH	C_0 [mg L ⁻¹]	Sorbent dosage [g L ⁻¹]	Contact time	Temperature [°C]
Effect of initial pH	ANA-Na-Ba, ANA-Ac-Na-Ba, ZSM5-Na-Ba	2,4,6,8,10	100	5	24 h	23
Effect of initial SO_4^{2-} concentration	ANA-Na-Ba	5–7	10–1000	5	3 h	10,23,40
	ANA-Ac-Na-Ba ZSM5-Na-Ba	3–4 4–7				
Effect of sorbent dosage	ANA-Na-Ba	5–7	100	1–25	2 h	10,23,40
	ANA-Ac-Na-Ba	3–4				
	ZSM5-Na-Ba	4–7				
Effect of contact time	ANA-Ac-Na-Ba	3–4	100	5	1 min – 24 h	23

ANA-Na-Ba: Barium-modified analcime, ANA-Ac-Na-Ba: Barium-modified acid-washed analcime, ZSM5-Na-Ba: Barium-modified commercial zeolite.

3

4 All sorption experiments were done duplicated. All samples were filtered through 0.45 μm filter
 5 paper (Sartorius Stedim Biotech) or separated using a centrifuge (3500 rpm, 5–15 min) before
 6 measurement of sulphate concentration by ion chromatography (Methrom 761 Compact IC).

7 **2.5 Adsorption isotherms**

8 Adsorption isotherms reveal the nature of the adsorption at varying initial concentrations in pH
 9 found to be optimal. The Langmuir, Freundlich, Dubinin-Raduschkevich, Temkin, Bi-Langmuir,
 10 Sips, Redlich–Peterson and Toth isotherm models were applied to the experimental data.
 11 Isotherm parameters were obtained using nonlinear regression with the Microsoft Excel (GRG
 12 nonlinear) solver tool.

13 The general non-linear form of Langmuir's [38] equation is

1

$$2 \quad q_e = \frac{b_L q_m C_e}{1 + b_L C_e}, \quad (3)$$

3

4 where q_e (mg g^{-1}) is the equilibrium adsorption capacity, q_m (mg g^{-1}) is the maximum adsorption
5 capacity of the adsorbent and b_L (L mg^{-1}) is a constant related to the adsorption energy [39].

6 The Freundlich [40] model can be written as

7

$$8 \quad q_e = K_F C_e^{1/n_F}, \quad (4)$$

9

10 where K_F (L mg^{-1}) is a relative indicator of adsorption capacity and dimensionless $1/n_F$ is the
11 measure of surface heterogeneity, which becomes more heterogeneous as the value gets closer
12 to zero [39].

13 The non-linear expression of the Dubinin-Radushkevich (D-R) isotherm model [41] can be
14 illustrated as Eqs. 5 and 6:

15

$$16 \quad q_e = q_m^{(-\beta \varepsilon^2)}, \quad (5)$$

$$17 \quad \varepsilon = RT \ln \left(1 + \frac{1}{C_e} \right), \quad (6)$$

18

19 where β ($\text{mol}^2 \text{J}^{-2}$) is a constant related to the mean free energy of adsorption per mole of the
20 ion and ε is the Polanyi potential. R , T and C_e represent the gas constant ($8.314 \text{ J mol}^{-1} \text{ K}^{-1}$),
21 absolute temperature (K) and adsorbate equilibrium concentration (mg L^{-1}), respectively [42].

22 The non-linear form of the Temkin isotherm [43] can be expressed by Eq. 7:

23

$$1 \quad q_e = B \ln A_T C_e, \quad (7)$$

2

3 where $B = (RT)/b_T$ is the Temkin constant related to the heat of the adsorption (J mol^{-1}), R (J mol^{-1}
 4 K^{-1}) is the gas constant, T (K) is the temperature, b_T is the Temkin isotherm constant and A_T (L
 5 g^{-1}) is the Temkin isotherm equilibrium binding constant [44].

6 The Bi-Langmuir isotherm [45] is presented in Eq. 8:

7

$$8 \quad q_e = \frac{q_{m1} b_{L1} C_e}{1 + b_{L1} C_e} + \frac{q_{m2} b_{L2} C_e}{1 + b_{L2} C_e}, \quad (8)$$

9

10 where q_{m1} and q_{m2} are the maximum adsorption capacities (mg g^{-1}) of two different adsorption
 11 sites. Similarly, b_{L1} and b_{L2} (mg g^{-1}) represent the energies of adsorption at these sites [46,47].

12 The Sips isotherm [48] is given as

13

$$14 \quad q_e = \frac{q_m (b_s C_e)^{n_s}}{1 + (b_s C_e)^{n_s}}, \quad (9)$$

15

16 where b_s (L mg^{-1}) is a constant related to the adsorption energy and n_s is a dimensionless
 17 constant characterising the heterogeneity of the system [49].

18 Redlich–Peterson (R–P) isotherm [50] can be calculated from Eq. 10:

19

$$20 \quad q_e = \frac{K_R C_e}{1 + a_R C_e^\beta}, \quad (10)$$

21

22 where K_R ($\text{dm}^3 \text{g}^{-1}$) and a_R ($\text{dm}^3 \text{mg}^{-1}$) are R–P isotherm constants and β is an exponent, the value
 23 of which lies between 0 and 1. For $\beta = 1$, the equation reduces to the Langmuir equation, with

1 $a_R = b_L$. At high adsorbate concentrations, the equation is transformed into the Freundlich
2 isotherm equation with $K_F = K_R/a_R$ and $1/n = 1-\beta$ [49, 51–54].

3 The Toth isotherm equation [55] can be written as in Eq. 11:
4

$$5 \quad q_e = \frac{q_m K_{Th} C_e}{[1+(K_{Th} C_e)^{Th}]^{1/Th}}, \quad (11)$$

6
7 where K_{Th} (mg dm^{-3}) is the Toth isotherm constant and Th is the dimensionless Toth isotherm
8 exponent, which characterises the heterogeneity of the system and is usually less than the unity.
9 The more Th deviates from the unity, the larger is the heterogeneity of the adsorbent. When Th
10 = 1, the Toth isotherm reduces to the Langmuir equation [51].

11 To evaluate the fit of the isotherm equations to the experimental data, the residual root
12 mean square error (RMSE) and the chi-square test (χ^2) were used. The smaller the error
13 function value, the better the curve fitting. The calculated expressions of error functions can be
14 defined as follows:

$$15 \quad \text{RMSE} = \sqrt{\frac{1}{n-p} \sum_{i=1}^n (q_{e(\text{exp})} - q_{e(\text{calc})})^2}, \quad (12)$$

$$16 \quad \chi^2 = \sum_{n=1}^n \frac{(q_{e(\text{exp})} - q_{e(\text{calc})})^2}{q_{e(\text{calc})}}, \quad (13)$$

17
18 where n is the number of experimental data, p is the number of parameters and $q_{e(\text{exp})}$ and $q_{e(\text{calc})}$
19 are the experimental and calculated values, respectively, of adsorption capacity in equilibrium
20 [44,56,57].
21
22

1 2.6 Kinetic modelling

2 The kinetics of the adsorption experiments was investigated by applying the experimental data
3 to pseudo-first-order, pseudo-second-order and Elovich models. The pseudo-first-order
4 equation [58] is

$$5 \log(q_e - q_t) = \log q_e - \frac{k_f}{2.303} t, \quad (14)$$

7 where q_e (mg g⁻¹) and q_t (mg g⁻¹) are the amounts of ions adsorbed at equilibrium and at time t
8 (min), respectively. k_f (min⁻¹) is the pseudo-first-order rate constant.

10
11 The linear form of the pseudo-second-order equation [59] is

$$13 \frac{t}{q_t} = \frac{1}{k_s q_e^2} + \frac{1}{q_e} t, \quad (15)$$

14
15 where k_s is the pseudo-second-order rate equilibrium constant (g mg⁻¹ min⁻¹). The linear form
16 of the Elovich equation from Zeldowitsch [60] is

$$18 q = \frac{1}{\beta} \ln \left(\nu_0 \beta + \frac{1}{\beta} \ln t \right), \quad (16)$$

19 where ν_0 (mg g⁻¹ min⁻¹) is the initial adsorption rate and β (g mg⁻¹) is the desorption constant
20 [61,62].

22 2.7 Thermodynamics of sorption

23
24 Thermodynamic constants including enthalpy change (ΔH), free energy change (ΔG) and
25 entropy change (ΔS) were calculated using Eqs. 17–19.

1 $\Delta G = -RT\ln(K),$ (17)

2 $K = \frac{q}{c_e},$ (18)

3 $\ln K = \frac{\Delta S}{R} - \frac{\Delta H}{RT},$ (19)

4 where ΔG is the free energy change (kJ mol⁻¹), ΔH is the change in enthalpy (kJ mol⁻¹), ΔS is the
5 entropy change (kJ mol⁻¹ K⁻¹), T is the absolute temperature (K) and R is the universal gas
6 constant (8.314 J mol⁻¹ K⁻¹) [51,63].

7

1 3 Results and discussion

2 3.1 Characterisation of the adsorbents

3 Chemical and mineral compositions of analcime (ANA) and commercial zeolite (ZSM-5) are
4 presented in Table 2. The main chemical constituents of the ANA are SiO₂ (46.55%), Al₂O₃
5 (19.31%) and Na₂O (9.66%) whereas ZSM-5 consists mainly of SiO₂ (77.43%) and Al₂O₃ (4.35%).
6 In addition, sorbents include some impurities and volatile compounds (e.g. water). According
7 to the results, Si/Al ratio of analcime is about 2.0, which is similar for the analcimes reported by
8 Atta *et al.* (2012) [12], Mallah *et al.* (2012) [13] and Liu *et al.* (2005) [64]. Si/Al ratio of
9 commercial zeolite (ZSM-5, CAS: 1318-02-1) is 15, which is similar with the XRF result.

10

11 Table 2. Main chemical constituents of analcime (ANA) and zeolite (ZSM-5) as determined by
12 XRF.

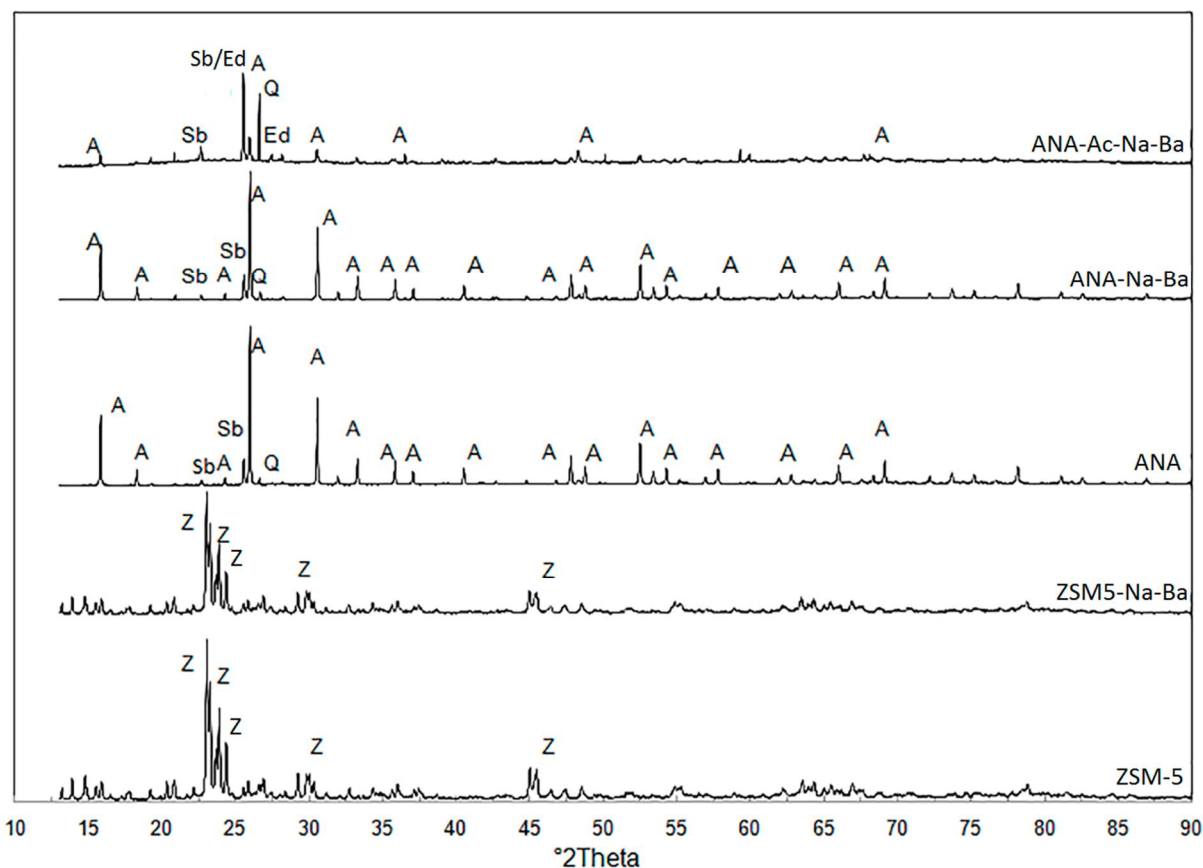
Composition	ANA [w/w%]	ZSM-5 [w/w%]
SiO ₂	46.55	77.43
Al ₂ O ₃	19.31	4.35
Na ₂ O	9.66	-
Fe ₂ O ₃	1.25	0.04
K ₂ O	0.45	0.001
CaO	0.38	0.02
Others ^a	0.23	0.05
LOI ^b	9.00	7.20

13 ^aIncluding Mn, Ti, Zn, Bi, Rb, Ga, Ni, Cr etc. ^bLoss on ignition (at 950 °C).

1 The XRD patterns of ANA, ANA-Na-Ba, ANA-Ac-Na-Ba, ZSM-5 and ZSM5-Na-Ba are shown in Fig.
2 1. The XRD patterns of ANA and ANA-Na-Ba indicate the presence of sodium aluminum silicon
3 oxide hydrate (analcime, $\text{Na}_8\text{Al}_8\text{Si}_{16}\text{O}_{48}(\text{H}_2\text{O})_8$, JCPDS 04-009-3254) and silicon oxide (quartz,
4 SiO_2 , 01-070-3755). In addition, they might also contain lithium aluminum silicate (spodumene,
5 $\text{LiAlSi}_2\text{O}_6$, 00-035-0797). The XRD pattern for commercial zeolite (ZSM-5, ammonium treated)
6 indicate the structure of hydrogen aluminum silicate hydrate ($\text{H}_{6.9}\text{Al}_{6.9}\text{Si}_{89.1}\text{O}_{192}(\text{H}_2\text{O})_{38}$, 04-013-
7 2411). As can be seen from Fig. 1, it seems that barium modification did not change the
8 chemical structure of ANA and ZSM-5. However, acid washing and further barium modification
9 changed the structure of ANA. Acid treatment is generally employed to oxidise the surface of
10 adsorbent, and it increases the acidity, removes the mineral elements and improves the
11 hydrophilic nature of the surface [2]. Fig 1 shows that acid treatment analcime (ANA-Ac-Na-Ba)
12 might also exhibit barium silicon aluminum oxide hydrate (edingtonite,
13 $\text{Ba}_{0.89}(\text{Si}_{3.04}\text{Al}_{1.96})\text{O}_{10}(\text{H}_2\text{O})_{3.32}$, 01-075-4005). However, it is quite difficult to distinguish
14 edingtonite with spodumene, because the highest peak of edingtonite (211), 2θ of 25.4° is
15 overlapped with spodumene (201), 2θ of 25.5° .

16 XRD results support results in Table 3. Barium modification has no significant effect on
17 surface area, pore sizes, and volumes. However, the surface area and pore volumes clearly
18 increase as a result of acid treatment and further barium modification in the case of analcime.
19 In the literature, it has been reported that acid treatment increases the specific surface area
20 and microporosity and reduces the cation-exchange capacity. This is due to that acid treatment
21 can remove impurities that block the pores, progressively eliminate cations into H-form and
22 finally dealuminate the structure [2,65,66].

23



1

2 Figure 1. X-ray diffraction patterns of ANA-Ac-Na-Ba, ANA-Na-Ba, ANA, ZSM5-Na-Ba and ZSM-
3 5. A: Analcime, Sb: Spodumene, Ed: Edingtonite, Q: Quartz, Z: Zeolite.

4

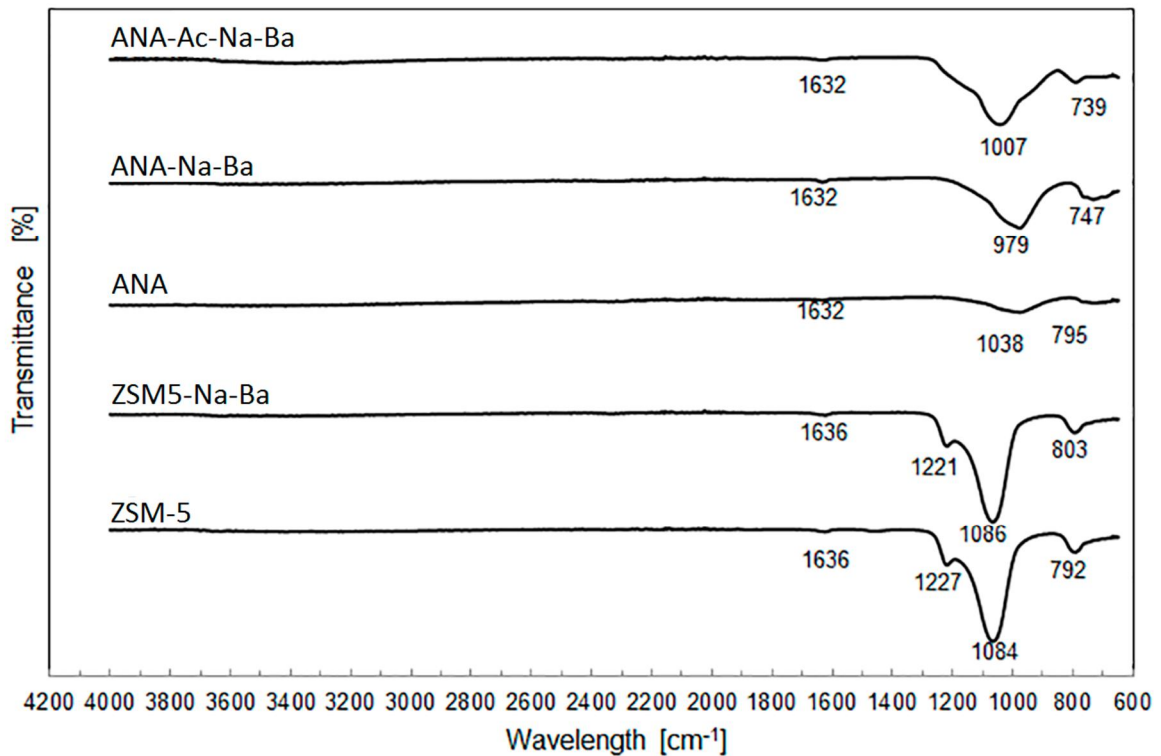
5

6 Table 3. Surface areas and pore volumes of raw materials (analcime and commercial zeolite)
7 and modified zeolite materials.

Sorbent	Specific surface area [m ² g ⁻¹]	V _{macro+meso} [cm ³ g ⁻¹]	V _{micro} [cm ³ g ⁻¹]	V _{total} [cm ³ g ⁻¹]	Pore size [average, nm]
ANA	3.01	0.007	0.0003	0.008	9.99

ANA-Na-Ba	2.27	0.008	0.0002	0.009	15.17
ANA-Ac-Na-Ba	238.42	0.133	0.034	0.160	2.68
ZSM-5	321.61	0.252	0.022	0.274	3.41
ZSM5-Na-Ba	327.72	0.259	0.026	0.285	3.48

1
2 The FT-IR spectra of ANA, ANA-Na-Ba, ANA-Ac-Na-Ba, ZSM-5 and ZSM5-Na-Ba are shown in Fig.
3 2. The bands at 1632–1636 cm⁻¹ are associated with water in the structure of the analcime and
4 zeolite materials. The bands in the spectra of the materials appearing between 979–1086 cm⁻¹
5 are related to the internal, anti-symmetric T–O (T = Al, Si) vibrations in tetrahedra or aluminio-
6 and silico-oxygen bridges. The bands between 739 and 803 cm⁻¹ belong to T–O (T = Al, Si)
7 symmetric stretching vibrations [1,15,67,68].

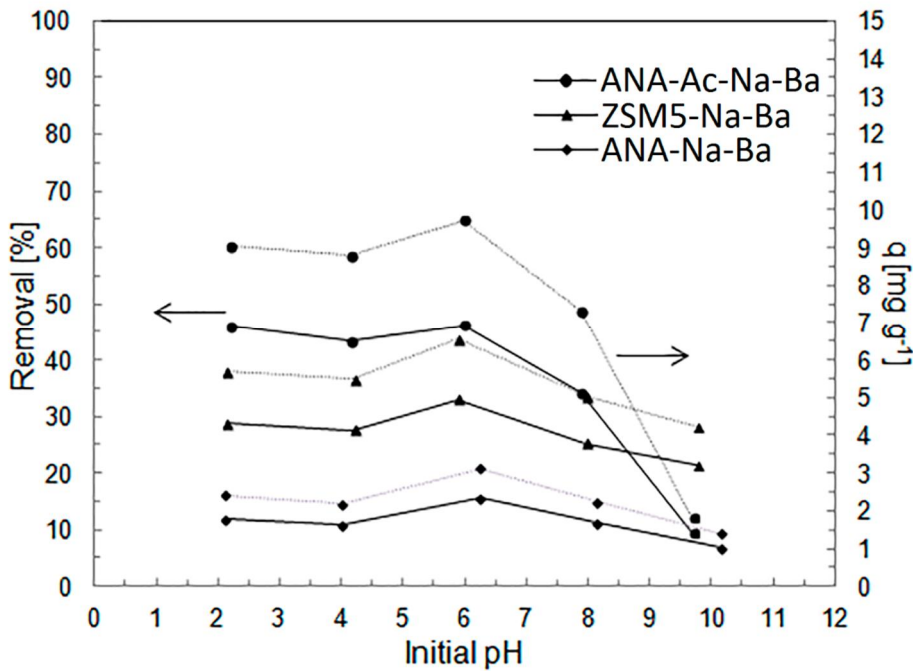


1
2 Figure 2. FT-IR spectrum of ANA-Ac-Na-Ba, ANA-Na-Ba, ANA, ZSM5-Na-Ba and ZSM-5.

3 **3.2** Effect of initial pH

4 First, the effect of initial pH in the range of 2–10 was studied for the produced sorbents. The
5 SO_4^{2-} ion removal efficiencies of the studied samples are shown in Fig. 3. In all cases, the
6 sorption capacity starts to slowly decrease after the initial pH value exceeds 6. Especially in the
7 case of ANA-Ac-Na-Ba removal, efficiency is better when the initial pH is lower than or equal to
8 6. The most probable reason for better removal under acidic conditions is the highly-protonated
9 surface of sorbents in an acidic medium, which tends to adsorb negative ions. In addition, the
10 large amount of OH^- competes with the SO_4^{2-} for unoccupied surface sites at a higher pH, which
11 decreases the sorption of SO_4^{2-} [28,51,69,70]. In further experiments of this paper, initial pH

1 values for ANA-Na-Ba, ANA-Ac-Na-Ba, and ZSM5-Na-Ba were in the ranges of 5–7, 3–4, and 4–
 2 7, respectively. These pH ranges were optimal for maximum sulphate removal (Fig. 3). For ANA-
 3 Ac-Na-Ba, the initial pH was adjusted to 3–4 because pH increased one or two units during the
 4 adsorption experiment.

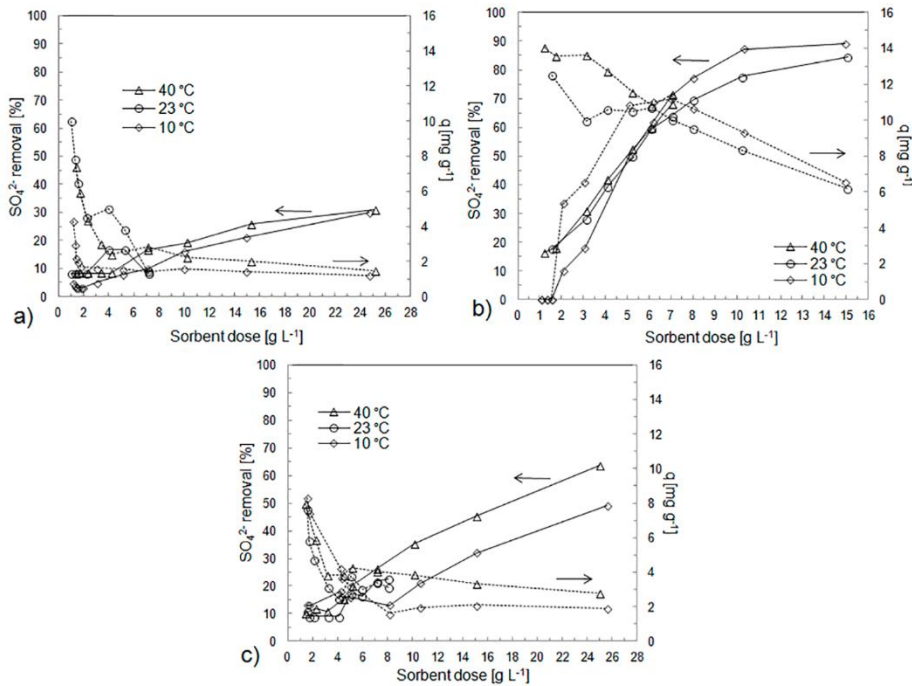


5
 6 Figure 3. Total SO_4^{2-} removal per cent (left, solid lines) and total adsorbed amount (right, dashed
 7 lines) versus initial pH on the sorption of SO_4^{2-} onto ANA-Na-Ba, ANA-Ac-Na-Ba and ZSM5-Na-
 8 Ba. Sorbent dose: 5 g L^{-1} , $C_0(\text{SO}_4^{2-})$: 100 mg L^{-1} , contact time: 24 h, temperature: 22–23 °C.

9 3.3 Effect of sorbent dose

10 The effect of ANA-Na-Ba, ANA-Ac-Na-Ba and ZSM5-Na-Ba dose on the sorption of SO_4^{2-} at
 11 different temperatures (10, 23, 40 °C) is shown in Fig. 4. The sorption capacities (q_e) decrease
 12 when the sorbent dose increases (dashed lines in Fig. 4), which can be explained by the increase

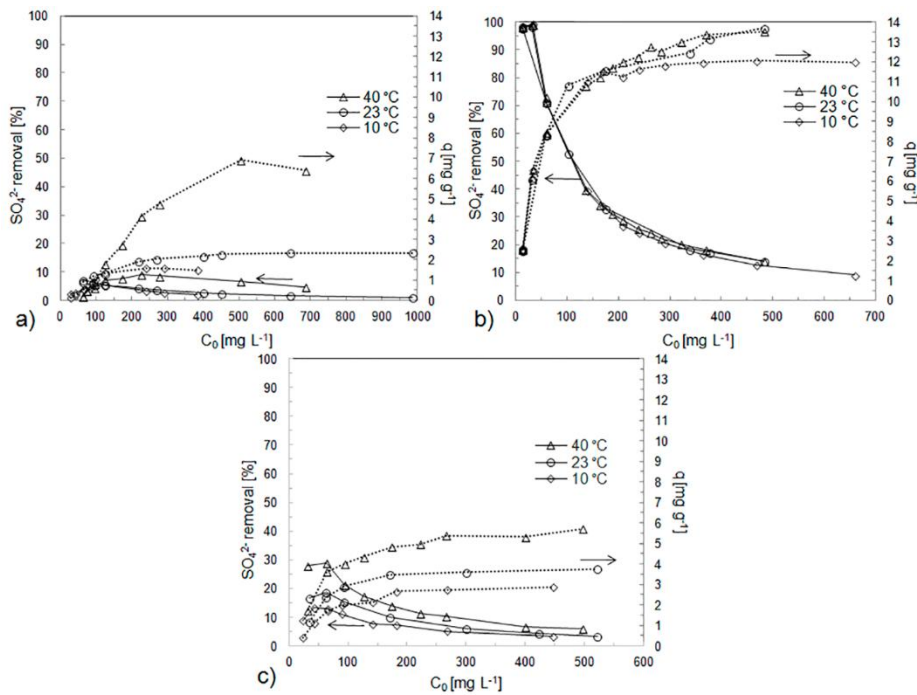
1 in the sorbent to adsorbate ratio. The higher the dosage, the greater the number of available
 2 adsorption sites there are against the SO_4^{2-} ions. This leads to the unsaturation of the sorption
 3 sites and results in comparatively less sorption amount at a higher sorbent dosage. The
 4 differences between sorption capacities at different temperatures are very minor, but it seems
 5 that sorption is more efficient at higher temperatures in all cases [51, 71–73].



6
 7 Figure 4. Effect of sorbent dosage on SO_4^{2-} removal at different temperatures (10, 23, 40 °C). a)
 8 ANA-Na-Ba, initial pH: 5–7; b) ANA-Ac-Na-Ba, initial pH: 3–4; and c) ZSM5-Na-Ba, initial pH: 4–
 9 7. Removal % of SO_4^{2-} is marked with a solid line, and sorption capacities (q) are marked with a
 10 dashed line. In all cases, $C_0(\text{SO}_4^{2-})$: $\sim 100 \text{ mg L}^{-1}$, contact time: 3 h and temperature: 22–23 °C.

1 **3.4** Effect of initial SO_4^{2-} concentration

2 The effect of SO_4^{2-} concentration was studied at three temperatures. The SO_4^{2-} uptake
3 mechanism is particularly dependent on the initial SO_4^{2-} concentration: at low concentrations,
4 SO_4^{2-} are sorbed by specific sites, while with increasing SO_4^{2-} concentrations the specific sites
5 are saturated and the exchange sites are filled [69,70]. In the case of SO_4^{2-} removal by ANA-Na-
6 Ba at 10 and 40 °C, removal efficiency (%) increases as initial concentration increases but then
7 starts to decrease. This phenomenon occurs due to the increased of a driving force provided by
8 the concentration gradient when the initial SO_4^{2-} concentration in the solution is increased [69].
9 The sorption capacities (q , mg g^{-1}) and removal efficiencies (%) increase as temperature is
10 increased. The same phenomenon has been seen in sorbent dose optimisation studies. This
11 indicates that sorption is an endothermic in nature. However, differences between sorption
12 capacities and removal efficiencies at different temperatures are minor, especially at low initial
13 concentrations. The probable removal mechanism of SO_4^{2-} on the zeolite materials is based on
14 the surface complexation or precipitation of extremely low solubility of BaSO_4 [2,17]. Fig. 5
15 shows the effect of SO_4^{2-} concentration on the removal and sorption capacity of SO_4^{2-} at these
16 temperatures.



1

2 Figure 5. Effect of initial concentration on SO_4^{2-} removal at different temperatures (10, 23,
 3 40 °C). a) ANA-Na-Ba, initial pH: 5–7; b) ANA-Ac-Na-Ba, initial pH: 3–4; and c) ZSM5-Na-Ba, initial
 4 pH: 4–7. Removal % of SO_4^{2-} is marked with a solid line, and sorption capacities (q) are marked
 5 with a dashed line. In all cases, sorbent dosage: 5 g L⁻¹ and contact time: 2 h.

6 3.5 Adsorption isotherms

7 Langmuir, Freundlich, D-R, Temkin, Bi-Langmuir, Sips, R-P and Toth isotherm models were
 8 applied for the experimental results of ANA-Na-Ba, ANA-Ac-Na-Ba and ZSM5-Na-Ba. Isotherm
 9 parameters, errors and graphs are shown in supplementary material. Comparison of the errors
 10 (RMSE, χ^2) and correlation coefficients (R^2) indicated that the SO_4^{2-} sorption onto ANA-Na-Ba
 11 and ZSM5-Na-Ba can be best represented by the Sips model at the temperatures 10 and 40 °C
 12 while the R–P and Sips models were favourable at 23 °C. This is logical result because Sips model
 13 is known to be applicable to the porous materials. In the case of ANA-Ac-Na-Ba, Bi-Langmuir

1 showed the best fit at all studied temperatures, which indicates monolayer adsorption to two
2 kind of sorption sites. The difference between the indicating values of the models was relatively
3 small when best models were compared. However, differences were quite large between the
4 best and the worst models. The maximum experimental sorption capacities were 2.3, 13.7 and
5 3.8 mg g⁻¹ for ANA-Na-Ba, ANA-Ac-Na-Ba and ZSM5-Na-Ba, respectively, at room temperature.
6 ANA-Ac-Na-Ba was the best sorbent and it was compared with sorbents reported in other
7 studies (Table 4). The adsorption capacities of the barium-modified acid-washed analcime
8 (ANA-Ac-Na-Ba) in SO₄²⁻ removal are comparable with values presented in the literature.

9

10

1 Table 4. Comparison of adsorption capacity q_m (mg g⁻¹) of various sorbents for the removal of
 2 SO₄²⁻ from aqueous phase.

Sorbent	Capacity q [mg g ⁻¹]	Initial pH	C ₀ [mg L ⁻¹]	Sorbent dose [g L ⁻¹]	Time [h/min]	T [°C]	Ref.
Surfactant-modified palygorskite	3.24 ^a	4	20–130 ^c	10	4 h	35	[28]
ZnCl ₂ activated coir pith carbon	4.9 ^a	4	20–80 ^c	10	30 min	35	[74]
Surfactant-modified clinoptilolite	~ 7.0 ^a	4.0–5.1	96–500 ^c	-	8 h	25	[35]
γ-Al ₂ O ₃	7.7	5.7	20–40 ^c	-	24 h	25	[75]
Surfactant-modified coir pith	8.76 ^a	2	10–50 ^c	4	-	32	[29]
Raw rice straw	11.68 ^a	6.4	50–500 ^c	2	2 h	25	[27]
Barium-modified acid- washed analcime	13.7 ^b	3–6	10–500 ^c	5	2 h	20–23	<i>This study</i>
Limestone	23.7 ^a	9.6–9.8	588–3000 ^d	25	9 h	23	[26]
Alkali-treated fly ash	43 ^a	-	200 ^e	-	~ 4 h	-	[76]
Epichlorohydrin and trimethylamine modified rice straw	74.76 ^a	6.4	50–500 ^c	2	2 h	25	[27]
Poly(<i>m</i> - phenylenediamine)	108.5 ^a	1.75	500–4000 ^c	-	1 h	23	[31]
Ba-modified blast furnace-slag geopolymer	119 ^b	7–8	865 ^d	5	24	20–23	[37]
Chitin-based shrimp shells	156.0 ^a	4.3	2350 ^c	10	1 h	-	[77]

^aLangmuir maximum sorption capacity, $q_{m,calc}$. ^bExperimental maximum sorption capacity, $q_{m,exp}$. ^cSynthetic ^dMine effluent, ^eGround water.

1 3.6 Kinetic modelling

2 Kinetic modeling was performed only for the best sorbent, ANA-Ac-Na-Ba, at room
3 temperature. Sorption equilibrium was attained at approximately 1 min, and it remained
4 constant thereafter. Maximum SO_4^{2-} removal and sorption capacity were 99.1% and 6.3 mg g^{-1}
5 (Fig not shown). Pseudo-first-order, pseudo-second-order and Elovich models were applied to
6 the experimental data. Fits are shown in Fig. 6, and the corresponding kinetic parameters and
7 correlation coefficients are presented in Table 4. The correlation coefficient (R^2) of the pseudo-
8 second-order model was clearly higher than the R^2 values of the pseudo-first-order and Elovich
9 models. In addition, the experimental sorption capacity ($q_{e,exp}$) of the pseudo-second-order
10 model agrees with the calculated sorption capacity ($q_{e,calc}$), which means that the sorption of
11 SO_4^{2-} ions onto ANA-Ac-Na-Ba follows the pseudo-second-order kinetic model. This indicates
12 that the rate of the adsorption process depends on the amount of SO_4^{2-} and available
13 adsorption sites.

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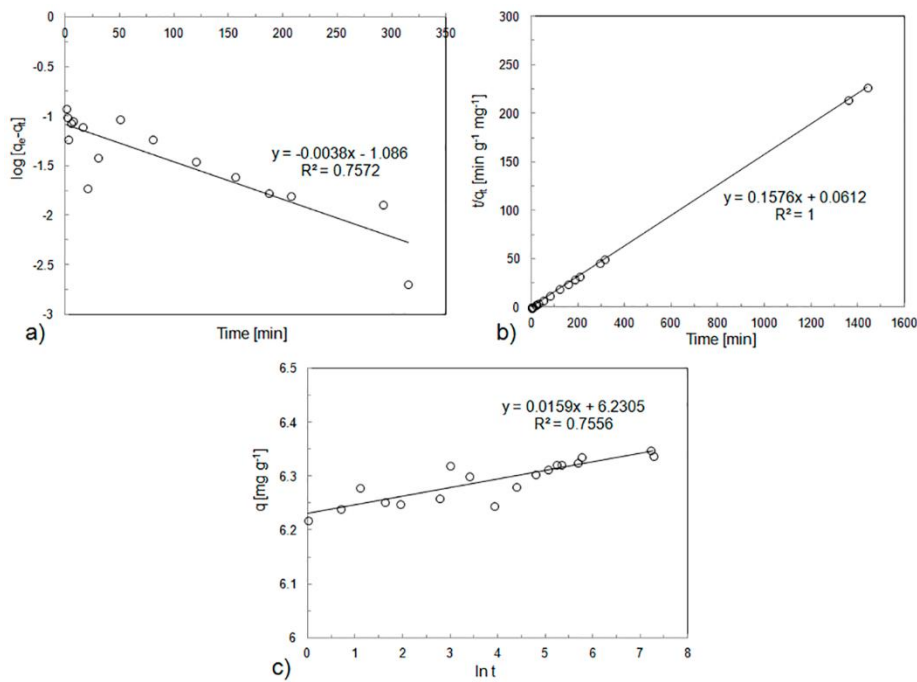
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1 Table 5. Pseudo-first-order, pseudo-second-order and Elovich model parameters for ANA-Ac-
 2 Na-Ba in SO₄²⁻ removal.

Experimental/Model	Constant [Unit]	Value
Experimental	Removal [%]	98.1
	q _{e(exp)} [mg g ⁻¹]	6.34
Pseudo-first-order	q _{e(cal)} [mg g ⁻¹]	0.08
	k ₁ [min ⁻¹]	0.009
	R ²	0.757
Pseudo-second-order	q _{e(cal)} [mg g ⁻¹]	6.35
	k ₂ [g mg ⁻¹ min ⁻¹]	0.406
	R ²	1
Elovich	β [g mg ⁻¹]	62.893
	u ₀ [mg g ⁻¹ min ⁻¹]	2.4E+168
	R ²	0.756

3



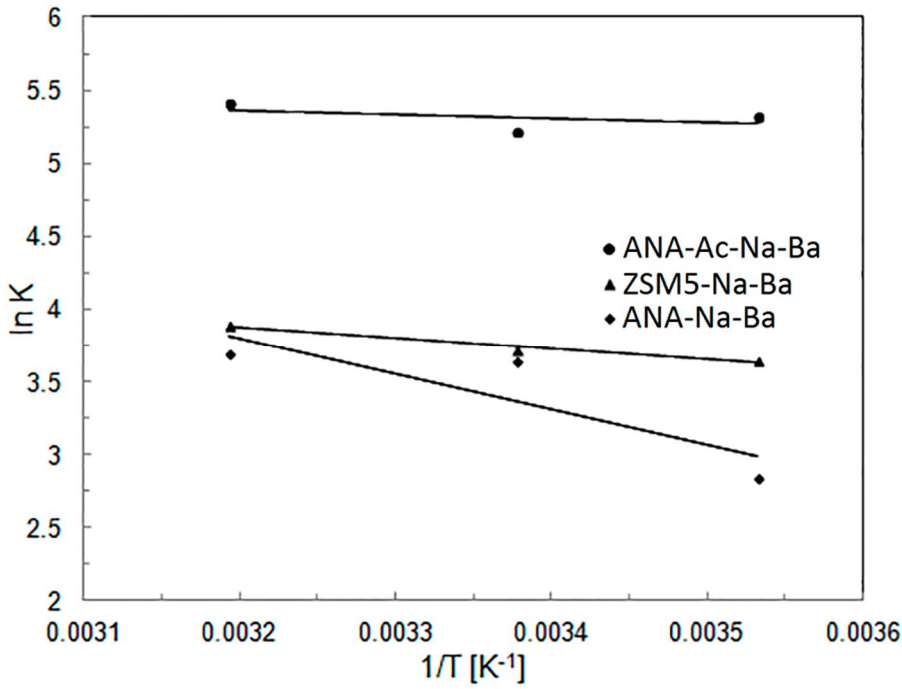
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2 Figure 6. a) Pseudo-first-order, b) pseudo-second-order and c) Elovich model plots of SO_4^{2-}
 3 removal ANA-Ac-Na-Ba. Adsorbate: model solution (C_0 , SO_4^{2-} : 100 mg L^{-1}), initial pH: 3–4,
 4 sorbent dose: 5 g L^{-1} , contact time: 24 h, and temperature: 20–23 °C.

5 3.7 Effect of temperature

6 Effect of temperature was studied by performing the experiments in three different
 7 temperatures (10, 20, 40 °C). As can be seen in Fig. 4 the rise of temperature increases the
 8 removal efficiency (%). However, the effect is minor. ΔH and ΔS values were obtained from the
 9 slope and intercept of the plot of $\ln Kc$ vs. $1/T$, as shown in Fig. 7 and listed in Table 5. The
 10 negative values of ΔG indicated that the sorption process was spontaneous in nature. The
 11 reaction is more spontaneous in the higher temperatures. The affinity of the modified sorbent
 12 materials for SO_4^{2-} are represented by the positive values of ΔS , which indicates that the
 13 sorption process increased the randomness at the solid/solution interface during the sorption

1 process. The positive values of ΔH suggest that the interaction of SO_4^{2-} and ANA-Na-Ba, ANA-
2 Ac-Na-Ba and ZSM5-Na-Ba is endothermic in nature. Because the ΔH values obtained in this
3 study are lower than 40 kJ mol^{-1} , the type of sorption is likely a physical process, involving weak
4 interactions [69, 70, 78–80].



5
6 Figure 7. Van't Hoff plots for the adsorption of SO_4^{2-} removal. Conditions: sorbent dose: 5 g L^{-1} ,
7 initial pH: 5–7 (ANA-Na-Ba), 3–4 (ANA-Ac-Na-Ba), 4–7 (ZSM5-Na-Ba), initial concentration: 100 mg L^{-1} .
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1 Table 6. Thermodynamic parameters for the sorption of SO_4^{2-} on ANA-Na-Ba, ANA-Ac-Na-Ba
 2 and ZSM5-Na-Ba at different temperatures.

Sorbent	Removal			$q_{m,exp}$			ΔG			ΔS	ΔH
	[%]			[mg g^{-1}]			[kJ mol^{-1}]			[$\text{J mol}^{-1} \text{K}^{-1}$]	[kJ mol^{-1}]
	10°C	23°C	40°C	10°C	23°C	40°C	10°C	23°C	40°C		
ANA-Na- Ba ^a	8.0	16.7	17.5	1.6	3.8	3.9	-6.7	-9.0	-9.6	96.7	20.4
ANA-Ac- Na-Ba ^b	51.8	50.0	55.0	10.8	10.5	11.6	-12.5	-12.8	-14.1	51.8	2.3
ZSM5-Na- Ba ^c	16.0	17.3	20.0	3.2	3.8	4.3	-8.6	-9.2	-10.1	51.2	6.0

Initial pH: a) 5–7, b) 3–4, c) 4–7. In all cases, sorbent dose: 5 g L^{-1} , initial SO_4^{2-} concentration: 100 mg L^{-1} .

3

4 Conclusions

5 Ba-modified analcime with (ANA-Ac-Na-Ba) and without acid-washing (ANA-Na-Ba) and Ba-
 6 modified ZSM-5 (ZSM5-Na-Ba) were studied for SO_4^{2-} removal. ANA-Ac-Na-Ba was found to be
 7 the most effective adsorbent of these three sorbent materials. The removal efficiencies were
 8 better at higher temperatures, indicating that adsorption is an endothermic process. Several
 9 isotherm models were applied to generate the experimental results of all sorbents. According
 10 to the results SO_4^{2-} sorption onto ANA-Ac-Na-Ba from model SO_4^{2-} solution can be best
 11 represented by the Bi-Langmuir at 10, 23 and 40°C , which indicates monolayer adsorption to
 12 two different kind of adsorption sites.

13 The results from the present study indicate that Ba-modified acid-washed analcime could
 14 be a feasible SO_4^{2-} sorbent in wastewater treatment (e.g. mining industry). Compared with the

1 adsorption capacities of other sorbents developed for SO_4^{2-} removal, the results obtained in this
2 study are in the same order of magnitude. Acid treatment and barium modification notably
3 increases the adsorption capacity of SO_4^{2-} compared with untreated or barium-modified
4 analcime.

5

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7

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4

1 Supplementary Data

2 Figure 1. Different isotherms of SO_4^{2-} on Ba-modified analcime (ANA-Na-Ba) at a) 10 °C, b) 23 °C
3 and c) 40 °C. Initial pH: 5–7, sorbent dosage: 5 g L⁻¹, contact time: 2 h.

4 Figure 2. Different isotherms of SO_4^{2-} on Ba-modified acid-washed analcime (ANA-Ac-Na-Ba) at
5 a) 10 °C, b) 23 °C and c) 40 °C. Initial pH: 3–4, sorbent dosage: 5 g L⁻¹, contact time: 2 h.

6 Figure 3. Different isotherms of SO_4^{2-} on Ba-modified commercial zeolite (ZSM5-Na-Ba) at a)
7 10°C, b) 23°C and c) 40°C. Initial pH: 4–7, sorbent dosage: 5 g L⁻¹, contact time: 2 h.

Table 1. Isotherm constants of models applied for SO_4^{2-} removal on ANA-Na-Ba, ANA-Ac-Na-Ba, and ZSM5-Na-Ba.

Experimental/ Model	Constant [unit]	ANA-Na-Ba			ANA-Ac-Na-Ba			ZSM5-Na-Ba		
		10 °C	23 °C	40 °C	10 °C	23 °C	40 °C	10 °C	23 °C	40 °C
Experimental Model	$q_m[\text{mg g}^{-1}]$	1.582	2.344	6.918	12.049	13.696	13.516	2.884	3.766	5.725
Langmuir	$q_m[\text{mg g}^{-1}]$	2.434	2.736	15.401	11.348	10.887	11.841	3.525	4.205	6.160
	$b_L [\text{L mg}^{-1}]$	0.0062	0.009	0.001	2.153	1.399	2.040	0.014	0.022	0.024
	R^2	0.874	0.976	0.894	0.834	0.870	0.811	0.946	0.929	0.961
	RMSE	0.216	0.089	0.882	1.546	1.670	1.653	0.214	0.275	0.257
	χ^2	0.473	0.0004	2.484	5.069	2.097	4.603	0.247	0.185	0.162
Freundlich	$K_F (\text{mg g}^{-1})$	0.070	0.376	0.055	5.419	4.827	5.448	0.335	0.829	1.232
	$1/n_F$	0.546	0.283	0.759	0.140	0.169	0.156	0.374	0.254	0.259
	R^2	0.797	0.857	0.857	0.886	0.922	0.934	0.869	0.817	0.852
	RMSE	0.274	0.219	1.028	1.282	1.291	0.974	0.371	0.479	0.503
	χ^2	0.696	0.195	2.974	3.166	1.997	2.922	0.582	0.489	0.539

Experimental/ Model	Constant [unit]	ANA-Na-Ba			ANA-Ac-Na-Ba			ZSM5-Na-Ba		
		10 °C	23 °C	40 °C	10 °C	23 °C	40 °C	10 °C	23 °C	40 °C
Dubinin- Raduschkevich	q_m [mg g ⁻¹]	1.638	2.233	6.960	11.707	12.241	12.392	2.661	3.644	5.144
	B [mol ² J ⁻²]	0.0007	0.0007	0.003	1.9E-5	1.8E-05	1.7E-05	0.0002	0.0002	0.0001
	R^2	0.975	0.908	0.982	0.604	0.592	0.505	0.942	0.989	0.983
	RMSE	0.096	0.176	0.368	2.389	2.959	2.677	0.222	0.118	0.401
	χ^2	1.269	0.195	2.122	2.259E	2.35E+	2.668E	0.408	0.030	0.272
				+156	147	+152				
Temkin	b_T	3600	4434.0	852.540	2126.2	2044.0	2104.0	2864.31	3064.5	2069.9
			95		42	69	35	6	3	08
	A_T [L g ⁻¹]	0.045	0.110	0.016	161.05	56.698	107.05	0.110	0.294	0.324
					9		7			
	R^2	0.898	0.926	0.966	0.904	0.916	0.928	0.936	0.877	0.918
	RMSE	0.194	0.158	0.502	1.174	1.341	1.020	0.233	0.393	0.374
χ^2	0.252	0.091	0.666	3.295	1.936	3.079	0.228	0.331	0.307	
Bi-Langmuir	q_{m1} [mg g ⁻¹]	2.436	1.367	7.051	8.515	7.246	7.837	1.762	2.103	3.080
	q_{m2} [mg g ⁻¹]	3.634	1.369	8.344	3.781	8.267	7.815	1.762	2.103	3.080
	b_{L1} [L mg ⁻¹]	0.006	0.009	0.001	0.066	0.005	4.591	0.014	0.022	0.024
	b_{L2} [L mg ⁻¹]	0	0.009	0.001	1E30	2.736	0.007	0.014	0.022	0.024
	R^2	0.874	0.976	0.894	0.924	0.954	0.947	0.946	0.929	0.961
	RMSE	0.256	0.106	1.043	1.174	1.216	0.950	0.262	0.355	0.304
	χ^2	0.472	0.031	2.484	2.804	1.082	2.396	0.247	0.185	0.162
Sips	q_m [mg g ⁻¹]	1.583	2.478	6.933	15.447	19.847	30.309	2.906	3.699	5.726
	b_s [L mg ⁻¹]	0.013	0.011	0.005	0.147	0.021	9.22E-	0.020	0.024	0.027
							04			
	n_s	3.186	1.393	2.779	0.321	0.289	0.217	1.674	2.102	1.300
R^2	0.989	0.990	0.991	0.910	0.943	0.934	0.976	0.995	0.970	

Experimental/ Model	Constant [unit]	ANA-Na-Ba			ANA-Ac-Na-Ba			ZSM5-Na-Ba		
		10 °C	23 °C	40 °C	10 °C	23 °C	40 °C	10 °C	23 °C	40 °C
	RMSE	0.070	0.061	0.277	1.201	1.216	1.014	0.157	0.080	0.247
	χ^2	0.105	0.015	0.166	3.262	1.660	2.997	0.082	0.009	0.108
Redlich– Peterson	K_R [L g ⁻¹]	0.022	0.019	0.017	55.593	35.911	111.15	0.036	0.059	0.130
							5			
	a_R [L mg ⁻¹]	5.00E-2	1.91E-3	3.93E-06	8.241	5.627	18.581	2.27E-3	2.64E-03	0.015
	B	0.730	1.189	1.823	0.900	0.883	0.862	1.251	1.273	1.053
	R ²	0.840	0.995	0.913	0.897	0.952	0.937	0.961	0.971	0.964
	RMSE	0.263	0.046	0.865	1.283	1.108	0.991	0.198	0.195	0.269
	χ^2	0.574	0.008	2.052	3.535	1.278	2.853	0.176	0.081	0.145
Toth	q_m [mg g ⁻¹]	1.546	2.420	6.663	18.124	49.304	122.33	2.912	3.668	5.750
							3			
	K_{Th} [mg L ⁻³] Th	0.007	0.007	0.003	912.00	689411	3.58E+	0.011	0.013	0.019
					0	.2	10			
	Th	31.561	1.746	64.355	0.196	0.100	0.063	1.993	3.049	1.350
	R ²	0.961	0.993	0.950	0.908	0.939	0.935	0.966	0.987	0.967
	RMSE	0.130	0.053	0.653	1.214	1.251	1.010	0.186	0.132	0.258
χ^2	0.211	0.012	1.702	3.290	1.697	2.983	0.148	0.036	0.126	